

# Towards a Scalable hp Adaptive Finite Element Code Based on a Non-Conformal Domain Decomposition Method

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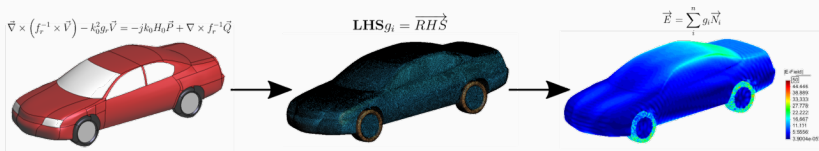
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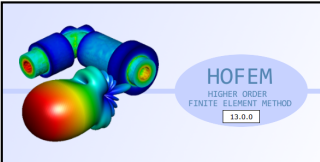
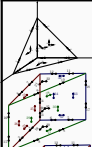

# Introduction

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- User-friendly.
- Based on GiD.

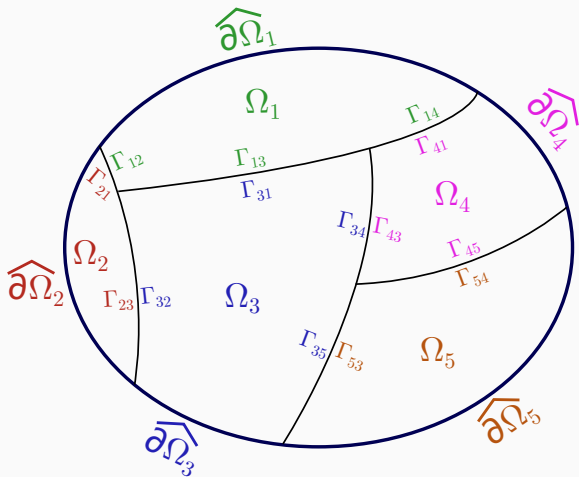


# Intro: design by blocks

		
MODULES		
DOMAIN	FAMILY	SOLVER
	Systematic	MUMPS
	Hierarchical	PARDISO

TESTS - MMS

- $h$  refinement.
- $p$  refinement.
- $hp$  refinement.



- Nonoverlapping, nonconformal and nonmatching.
- Hybrid meshes.
- Geometry aware optimization.
- *hp* adaptivity in 3D.

# Formulation

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$$\nabla \times \frac{1}{\mu_r} (\nabla \times \mathbf{E}) - k_0^2 \epsilon_r \mathbf{E} = \mathbf{0}$$

$$\hat{\mathbf{n}} \times \mathbf{E} = 0, \text{ on } \Gamma_D$$

$$\hat{\mathbf{n}} \times \frac{1}{\mu_{ri}} (\nabla \times \mathbf{E}) = 0, \text{ on } \Gamma_N$$

$$\hat{\mathbf{n}} \times \frac{1}{\mu_{ri}} (\nabla \times \mathbf{E}) + jk_0 \hat{\mathbf{n}} \times \hat{\mathbf{n}} \times \mathbf{E} = \Psi, \text{ on } \Gamma_C$$

## Formulation: variational formulation

Find  $\mathbf{E} \in \mathbf{W}$  such that

$$c_1(\mathbf{F}, \mathbf{E}) - k_0^2 c_2(\mathbf{F}, \mathbf{E}) + \gamma c_3(\mathbf{F}, \mathbf{E}) = l(\mathbf{F}), \quad \forall \mathbf{F} \in \mathbf{W}$$

$$c_1(\mathbf{F}, \mathbf{E}) = \int_{\Omega} (\nabla \times \mathbf{F}) \cdot \left( \frac{1}{\mu_r} \nabla \times \mathbf{E} \right) d\Omega$$

$$c_2(\mathbf{F}, \mathbf{E}) = \int_{\Omega} \mathbf{F} \cdot \varepsilon_r \mathbf{E} d\Omega$$

$$c_3(\mathbf{F}, \mathbf{E}) = \int_{\Gamma_C} (\hat{\mathbf{n}} \times \mathbf{F}) \cdot (\hat{\mathbf{n}} \times \mathbf{E}) d\Gamma_C$$

$$l(\mathbf{F}) = \int_{\Omega} (\mathbf{F} \cdot \mathbf{O}) d\Omega - \int_{\Gamma_C} (\mathbf{F} \cdot \boldsymbol{\Psi}) d\Gamma_C$$

$$\mathbf{W} := \{ \mathbf{A} \in \mathbf{H}(\text{curl}, \Omega), \hat{\mathbf{n}} \times \mathbf{A} = 0 \text{ on } \Gamma_D \}$$

$$\nabla \times \frac{1}{\mu_{ri}} (\nabla \times \mathbf{E}_i) - k_0^2 \varepsilon_{ri} \mathbf{E}_i = \mathbf{O}_i$$

$$\hat{\mathbf{n}}_i \times \mathbf{E}_i = 0, \text{ on } \Gamma_{i,D}$$

$$\hat{\mathbf{n}}_i \times \frac{1}{\mu_{ri}} (\nabla \times \mathbf{E}_i) = 0, \text{ on } \Gamma_{i,N}$$

$$\hat{\mathbf{n}}_i \times \frac{1}{\mu_{ri}} (\nabla \times \mathbf{E}_i) + jk_0 \hat{\mathbf{n}}_i \times \hat{\mathbf{n}}_i \times \mathbf{E}_i = \Psi_i, \text{ on } \Gamma_{i,C}$$

$$\hat{\mathbf{n}}_i \times \mathbf{E}_i \times \hat{\mathbf{n}}_i = \hat{\mathbf{n}}_j \times \mathbf{E}_j \times \hat{\mathbf{n}}_j, \text{ on } \Gamma_{ij}$$

$$\hat{\mathbf{n}}_i \times \frac{1}{\mu_{ri}} (\nabla \times \mathbf{E}_i) = -\hat{\mathbf{n}}_j \times \frac{1}{\mu_{rj}} (\nabla \times \mathbf{E}_j), \text{ on } \Gamma_{ij}$$

## Formulation: cement variables and TC

$$\begin{aligned}\mathbf{e}_i &= \hat{\mathbf{n}}_i \times \mathbf{E}_i \times \hat{\mathbf{n}}_i \\ \mathbf{j}_i &= \frac{1}{k_0} \hat{\mathbf{n}}_i \times \frac{1}{\mu_{ri}} (\nabla \times \mathbf{E}_i) \\ \rho_i &= \frac{1}{k_0} \nabla_\tau \cdot \mathbf{j}_i\end{aligned}$$

$$\begin{aligned}(\alpha \mathcal{I} + \beta_i \mathcal{S}_{TE})(\mathbf{e}_i) + (\mathcal{I} + \gamma_i \mathcal{S}_{TM})(\mathbf{j}_i) = \\ (\alpha \mathcal{I} + \beta_j \mathcal{S}_{TE})(\mathbf{e}_j) - (\mathcal{I} + \gamma_j \mathcal{S}_{TM})(\mathbf{j}_j)\end{aligned}$$

$$\mathcal{S}_{TE} = \nabla_\tau \times \nabla_\tau \times$$

$$\mathcal{S}_{TM} = \nabla_\tau \nabla_\tau \cdot$$

## Formulation: variational formulation with DDM (i)

Find  $\mathbf{E}_i \in \mathbf{W}_i, \mathbf{j}_i \in \mathbf{X}_i, \rho_i \in Y_i$  such that

$$c_1(\mathbf{F}_i, \mathbf{E}_i) - k_0^2 c_2(\mathbf{F}_i, \mathbf{E}_i) + \\ jk_0 c_{\tau,1}(\widehat{\mathbf{n}}_i \times \mathbf{F}_i, \widehat{\mathbf{n}}_i \times \mathbf{E}_i) = l(\mathbf{F}_i), \quad \forall \mathbf{F}_i \in \mathbf{W}_i$$

$$\alpha c_{\tau,1}(\mathbf{l}_i, \mathbf{e}_i) + k_0 c_{\tau,1}(\mathbf{l}_i, \mathbf{j}_i) + k_0^2 \gamma_i c_{\tau,1}(\mathbf{l}_i, \nabla_{\tau} \rho_i) + \\ \beta_i k_0 c_{\tau,1}(\nabla_{\tau} \times \mathbf{l}_i, \nabla_{\tau} \times \mathbf{e}_i) = \alpha c_{\tau,1}(\mathbf{l}_i, \mathbf{e}_i) - \\ k_0 c_{\tau,1}(\mathbf{l}_i, \mathbf{j}_j) - k_0^2 \gamma_j c_{\tau,1}(\mathbf{l}_i, \nabla_{\tau} \rho_j) + \\ \beta_j k_0 c_{\tau,1}(\nabla_{\tau} \times \mathbf{l}_i, \nabla_{\tau} \times \mathbf{e}_j), \quad \forall \mathbf{l}_i \in \mathbf{X}_i$$

$$c_{\tau,1}(\nabla_{\tau} \phi_i, \mathbf{j}_i) + k_0 c_{\tau,2}(\phi_i, \rho_i) = 0, \quad \forall \phi_i \in Y_i$$

$$\mathbf{F}_i \in \mathbf{W}_i := \mathbf{H}_0(\text{curl}; \Omega_i), \quad \mathbf{l}_i \in \mathbf{X}_i := \mathbf{H}_0(\text{curl}_{\tau}; \Gamma_{ij}), \\ \phi_i \in Y_i := H_0^{-1/2}(\Gamma_{ij})$$

## Formulation: variational formulation with DDM (& ii)

$$c_1(\mathbf{F}_i, \mathbf{E}_i) = \int_{\Omega_i} (\nabla \times \mathbf{F}_i) \cdot \frac{1}{\mu_{ri}} (\nabla \times \mathbf{E}_i) d\Omega_i$$

$$c_2(\mathbf{F}_i, \mathbf{E}_i) = \int_{\Omega_i} \mathbf{F}_i \cdot \varepsilon_{ri} \mathbf{E}_i d\Omega_i$$

$$c_{\tau,1}(\mathbf{l}_i, \mathbf{e}_j) = \int_{\Gamma_{ij}} (\mathbf{l}_i \cdot \mathbf{e}_j) d\Gamma_{ij}$$

$$c_{\tau,2}(\phi_i, \rho_j) = \int_{\Gamma_{ij}} (\phi_i \rho_j) d\Gamma_{ij}$$

$$l(\mathbf{F}_i) = \int_{\Omega_i} (\mathbf{F}_i \cdot \mathbf{O}_i) d\Omega_i - \int_{\Gamma_{i,C}} (\mathbf{F}_i \cdot \boldsymbol{\Psi}_i) \Gamma_{i,C}$$

# Verification

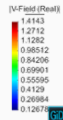
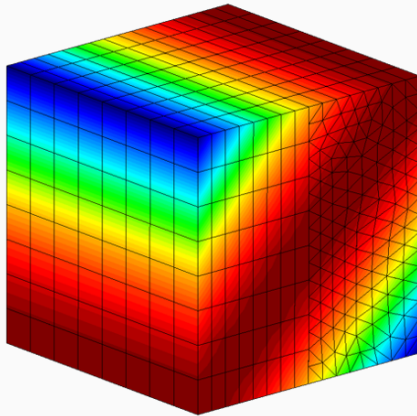
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## Verification: sources of error

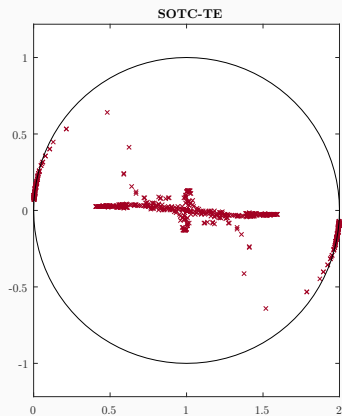
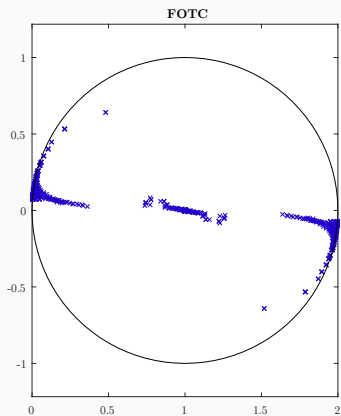
- Introduction of domains: user-driven or ParMETIS.
- Shapes.
- Orders.
- Nonmatching interfaces.



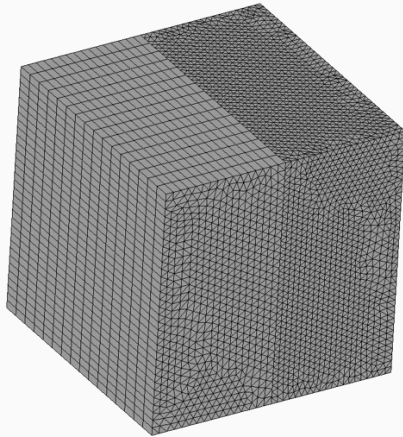
# Verification: hexahedra with prisms



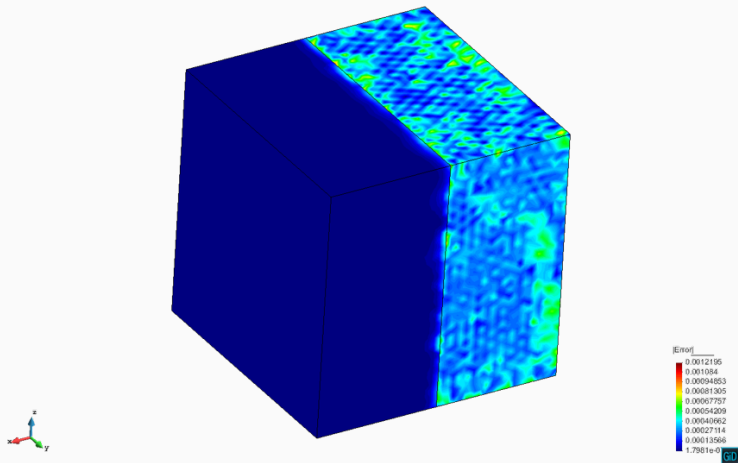
# Verification: hexahedra with prisms



# Verification: nonconformal in shape and order



# Verification: nonconformal in shape and order



## Numerical results

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# Results: setup

- Pre and postprocessing: GiD.
- Direct solver: MUMPS.
- Iterative solver: GCR through PETSC.
  - Residual:  $10^{-6}$ .
- SOTC-TE.

## Results: 2D circular horn array

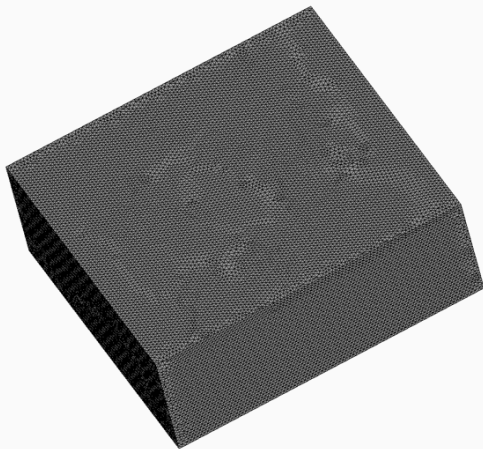
- 3x3 and 4x4 circular horns.
- Working frequency  $f = 10$  GHz
- Uniform excitation through WR-90 waveguides.
- Unstructured tetrahedra.

## Results: 2D circular horn array

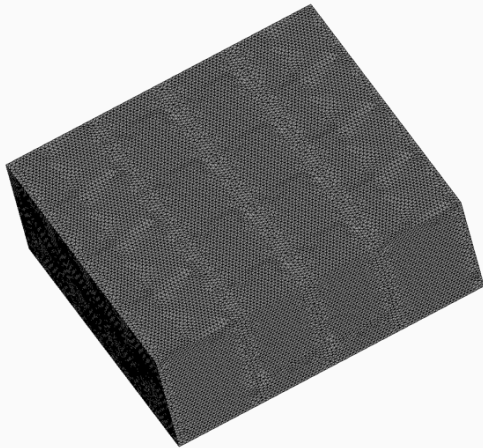
Case of study	Time (s)	Peak memory (Mb)	Unknowns	Surf. unkn	Iterations
3x3 No DDM	416	5380	1360188	—	—
3x3 DDM	463	3371	1398118	60144	62
4x4 No DDM	1579	12253	2261472	—	—
4x4 DDM	1191	5832	2368032	185856	73



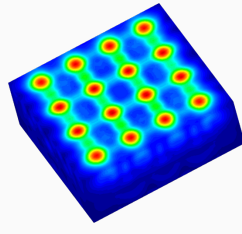
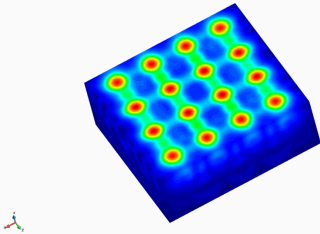
# Results: 2D circular horn array



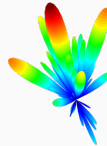
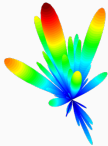
# Results: 2D circular horn array



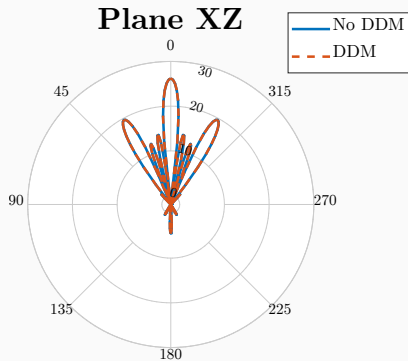
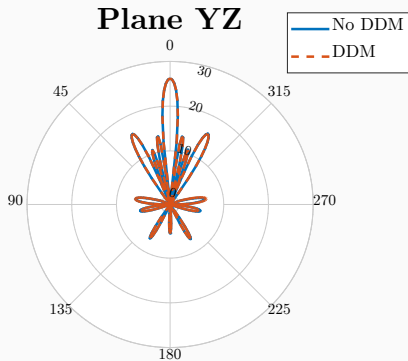
# Results: 2D circular horn array



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# Results: 2D circular horn array

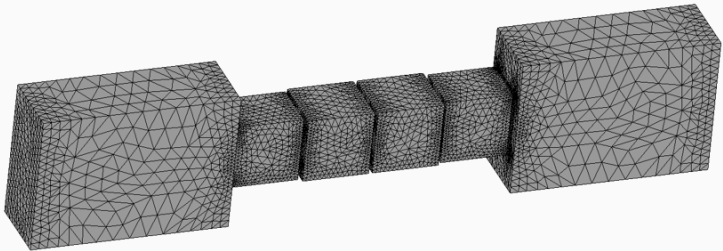


## Results: X-band waveguide filter

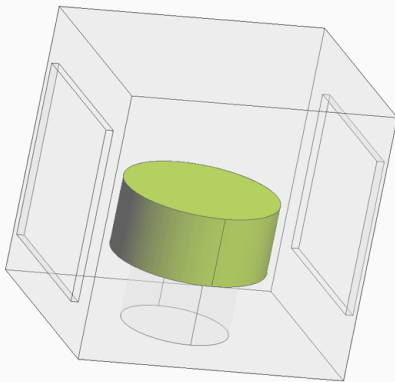
- WR-75 waveguide.
- X-band.
- 4 rectangular cavities:
  - Embedded resonator of  $\epsilon_r = 30$ .
  - Support of  $\epsilon_r = 9$ .
- 236690 unknowns for DDM, 412428 without DDM.

Alessandri, Ferdinando, et al. "The electric-field integral-equation method for the analysis and design of a class of rectangular cavity filters loaded by dielectric and metallic cylindrical pucks." *IEEE transactions on microwave theory and techniques*, 52.8 (2004): 1790-1797.

# Results: X-band waveguide filter



# Results: X-band waveguide filter

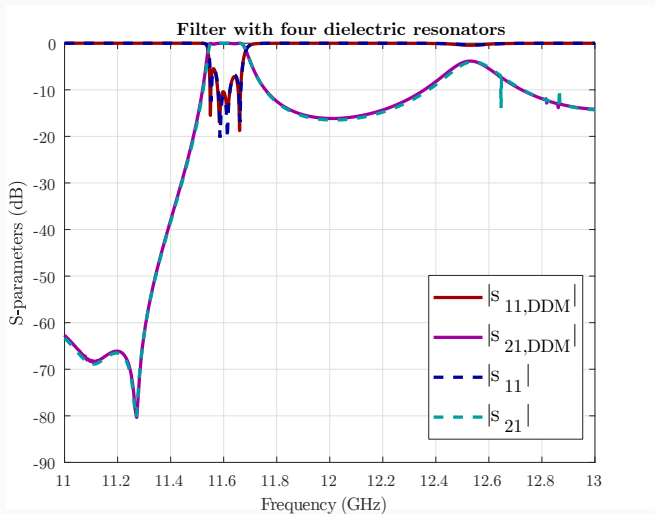




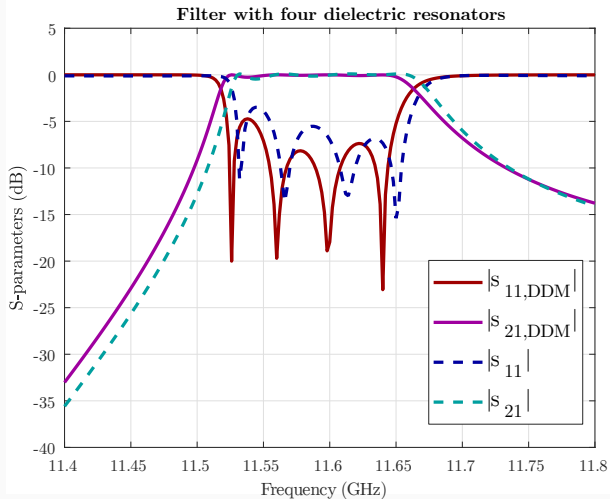
## Results: X-band waveguide filter

## Results: X-band waveguide filter

# Results: X-band waveguide filter



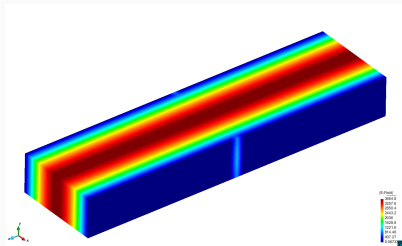
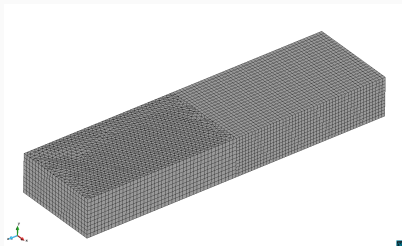
# Results: X-band waveguide filter



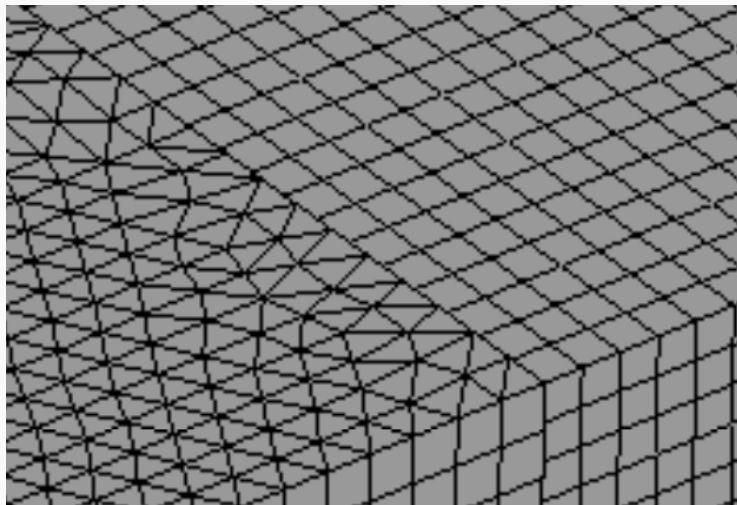
## h adaptivity: nonconformal waveguide

- WR-90 empty waveguide.
- Working frequency  $f = 7.5$  GHz.
- Length of  $10\lambda_g$ .

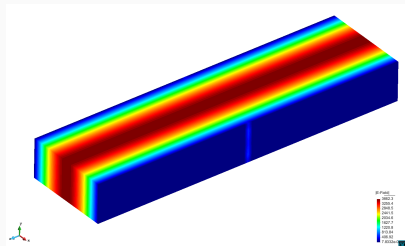
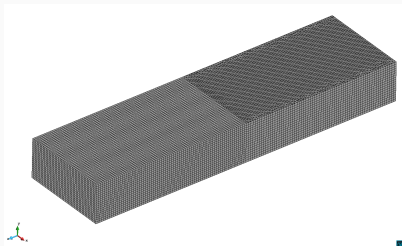
# h adaptivity: nonconformal waveguide



## h adaptivity: nonconformal waveguide



# h adaptivity: nonconformal waveguide





## h adaptivity: steps

- Solve.
- Estimate.
- Mark.
- Refine.

$$\mathcal{R}_{\text{vol},i}^{(m)} = \nabla \times \mu_{ri}^{(-1)} (\nabla \times \mathbf{E}_{i,\text{FEM}}^{(m)}) - k_0^2 \varepsilon_{ri} \mathbf{E}_{i,\text{FEM}}^{(m)} - \mathbf{O}_i,$$

$$\mathcal{R}_N^{(m)} = \hat{\mathbf{n}}_i^{(m)} \times \mu_{ri}^{(-1)} (\nabla \times \mathbf{E}_{i,\text{FEM}}^{(m)}), \quad \text{on } \Gamma_{i,N},$$

$$\mathcal{R}_C^{(m)} = \hat{\mathbf{n}}_i \times \mu_{ri}^{(-1)} (\nabla \times \mathbf{E}_{i,\text{FEM}}^{(m)}) +$$

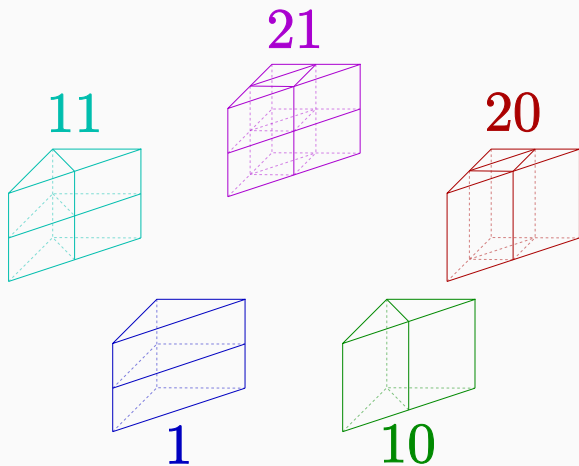
$$jk_0 \hat{\mathbf{n}}_i^{(m)} \times \hat{\mathbf{n}}_i^{(m)} \times (\Psi_i - \mathbf{E}_{i,\text{FEM}}^{(m)}), \quad \text{on } \Gamma_{i,C}.$$

$$\mathcal{R}_{i,\text{neigh}} \hat{\mathbf{n}}_i^{(m)} = \hat{\mathbf{n}}_i^{(m)} \times \mu_{ri}^{(-1)} (\nabla \times \mathbf{E}_{i,\text{FEM}}^{(m)}) + \hat{\mathbf{n}}_i^{(n)} \times \mu_{ri}^{(-1)} (\nabla \times \mathbf{E}_{i,\text{FEM}}^{(n)}).$$

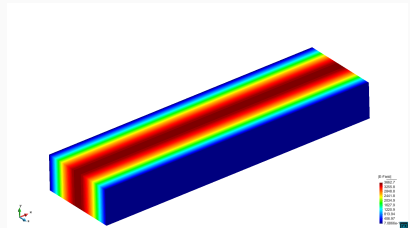
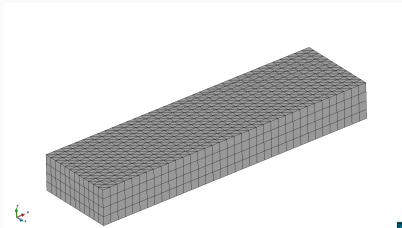
$$\mathcal{R}_{ij,\text{DDM}}^{(m)} = \pi_\tau(\mathbf{E}_{i,\text{FEM}}^{(m)}) + \pi_\tau^\times(\mu_{ri}^{(-1)} \nabla \times \mathbf{E}_{i,\text{FEM}}^{(m)}) -$$

$$\pi_\tau(\mathbf{E}_{j,\text{FEM}}^{(m)}) - \pi_\tau^\times(\mu_{rj}^{-1} \nabla \times \mathbf{E}_{j,\text{FEM}}^{(m)}).$$

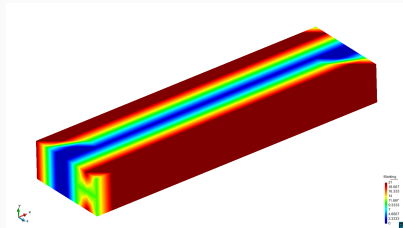
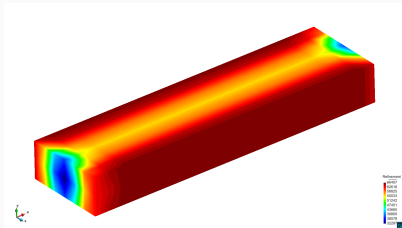
## h adaptivity: steps



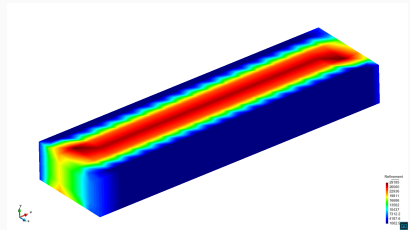
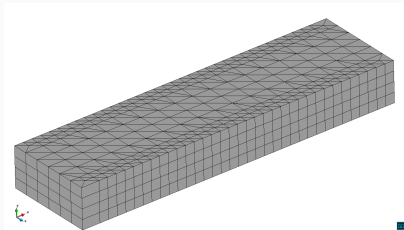
# h adaptivity: steps



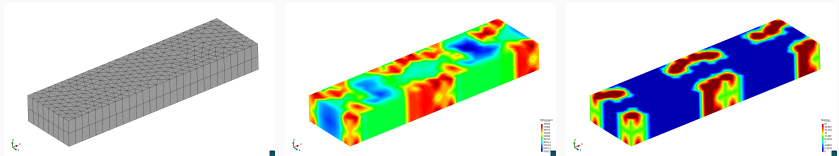
# h adaptivity: steps



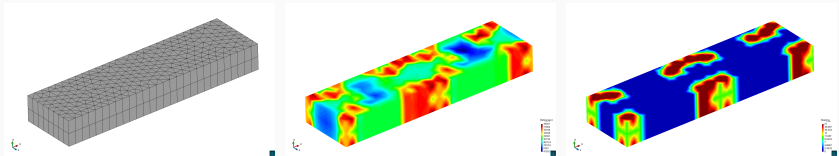
# h adaptivity: steps



# h adaptivity: unstructured mesh, no DDM

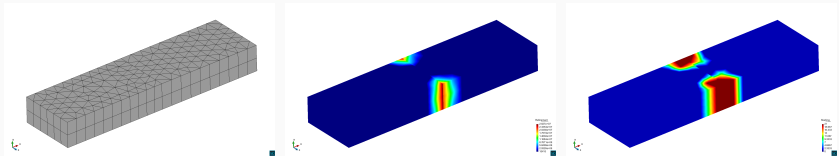


# h adaptivity: unstructured mesh, conformal DDM

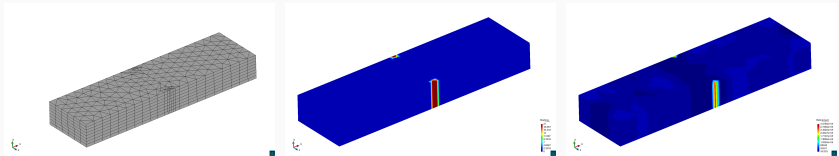




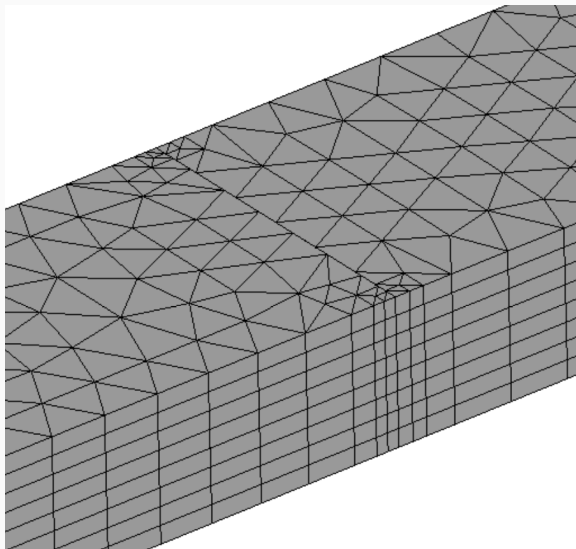
# h adaptivity: unstructured mesh, nonconformal DDM



# h adaptivity: unstructured mesh, nonconformal DDM

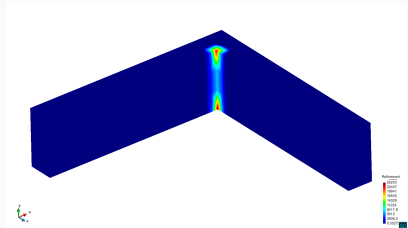
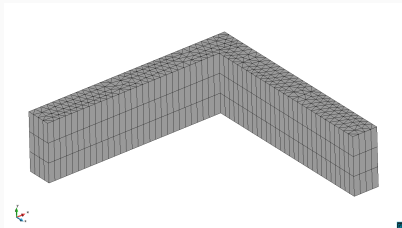


## h adaptivity: unstructured mesh, nonconformal DDM

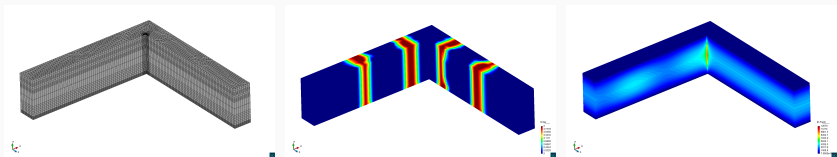


- Singularity through L-shape domain along E-plane.
- Working frequency  $f = 7.5$  GHz.
- WR-90 waveguide.

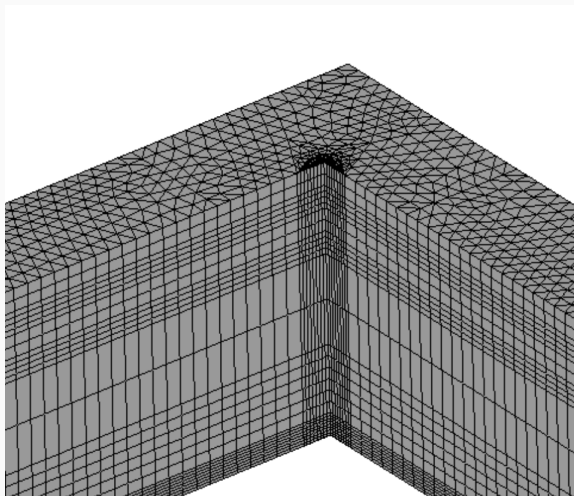
# Bonus track: hp adaptivity



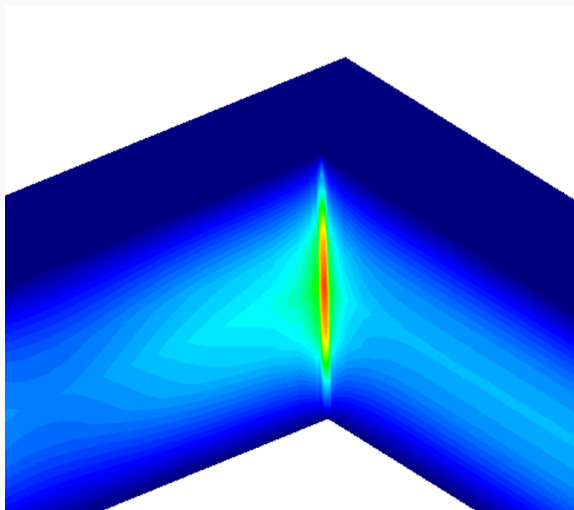
# Bonus track: hp adaptivity



## Bonus track: hp adaptivity

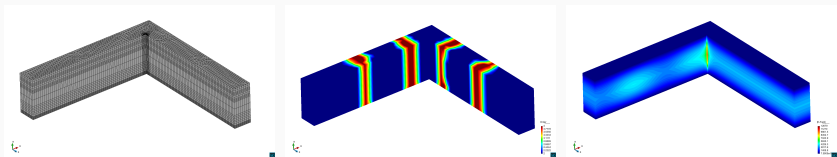


## Bonus track: hp adaptivity





# Bonus track: hp adaptivity



# Conclusions

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- Introduction of DDM for hp refinement meshes.
- Geometry aware optimization with hybrid meshes.
- Best use of memory.
- Nonconformal study of adaptivity.

Thanks for your attention!

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